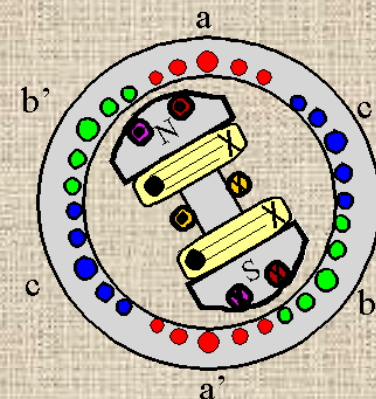
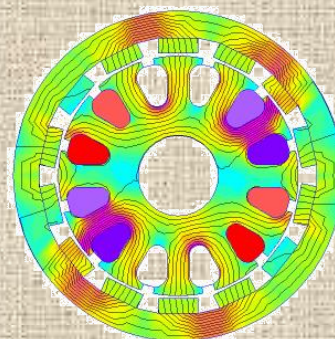
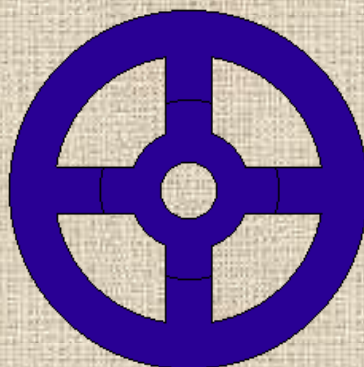
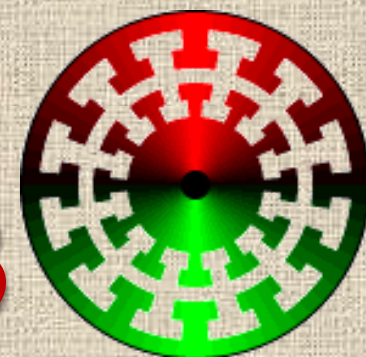
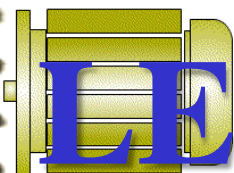


# EE552 ELECTRICAL MACHINES III

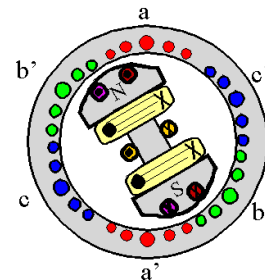


## LECTURE 13



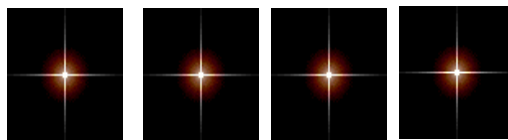


# LECTURE NOTES



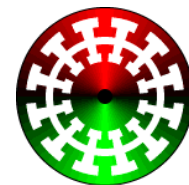
## ELECTRICAL MACHINES III

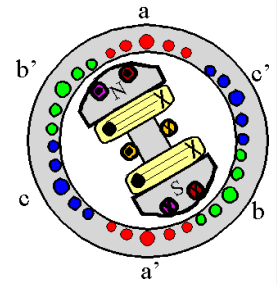
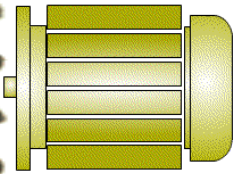
EE552



SPRING 2018

Dr : MUSTAFA AL-REFAI

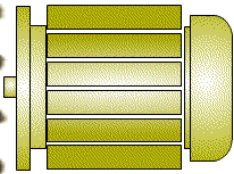




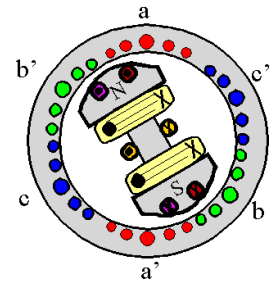
# LECTURE 13

## SYNCHRONOUS GENERATOR





# Measuring parameters of synchronous generator model



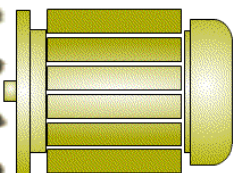
The three quantities must be determined in order to describe the generator model:

1. The relationship between field current and flux (and therefore between the field current  $I_F$  and the internal generated voltage  $E_A$ );
2. The synchronous reactance;
3. The armature resistance.

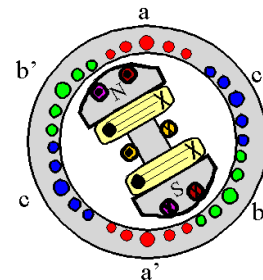
## OPEN CIRCUIT TEST (OCC)

We conduct first the **open-circuit test** on the synchronous generator: the generator is rotated at the rated speed, all the terminals are disconnected from loads, the field current is set to zero first. Next, the field current is increased in steps and the phase voltage (which is equal to the internal generated voltage  $E_A$  since the armature current is **zero**) is measured.

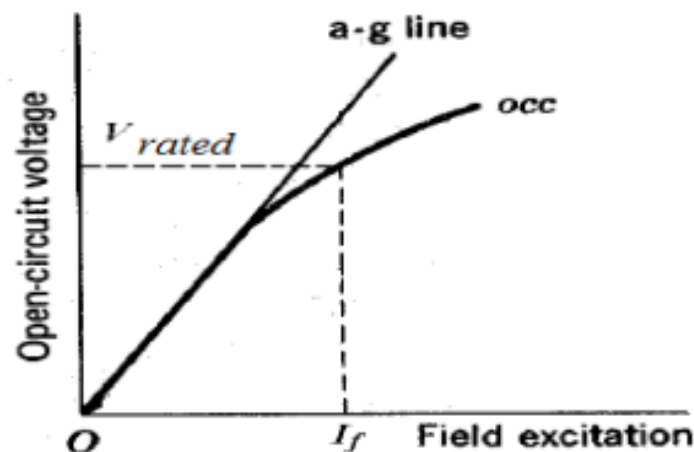
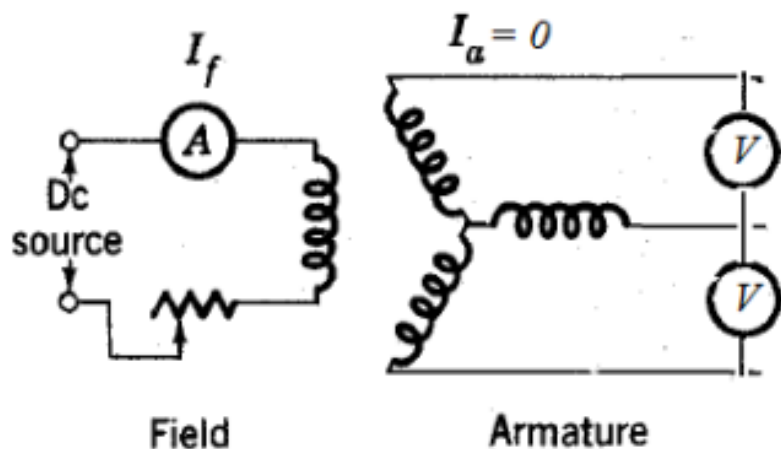




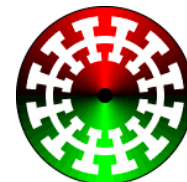
# Open-Circuit Characteristic (OCC)



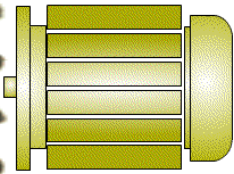
Therefore, it is possible to plot the dependence of the internal generated voltage on the field current – the **open-circuit characteristic (OCC)** of the generator.



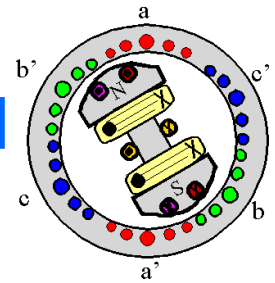
**Open-Circuit Characteristic (O.C.C.)**



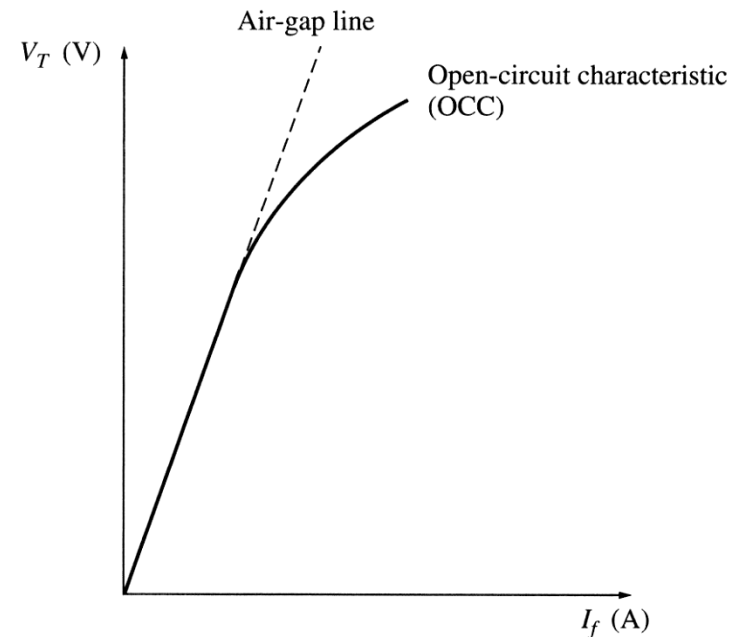




# Measuring parameters of synchronous generator model



Since the unsaturated core of the machine has a reluctance **thousands times** lower than the reluctance of the air-gap, the resulting flux increases linearly first. When the saturation is reached, the core reluctance greatly increases causing the flux to increase much slower with the increase of the **mmf**.

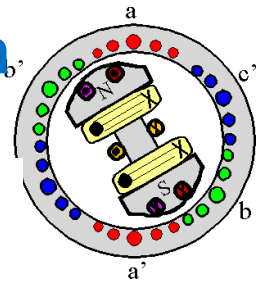
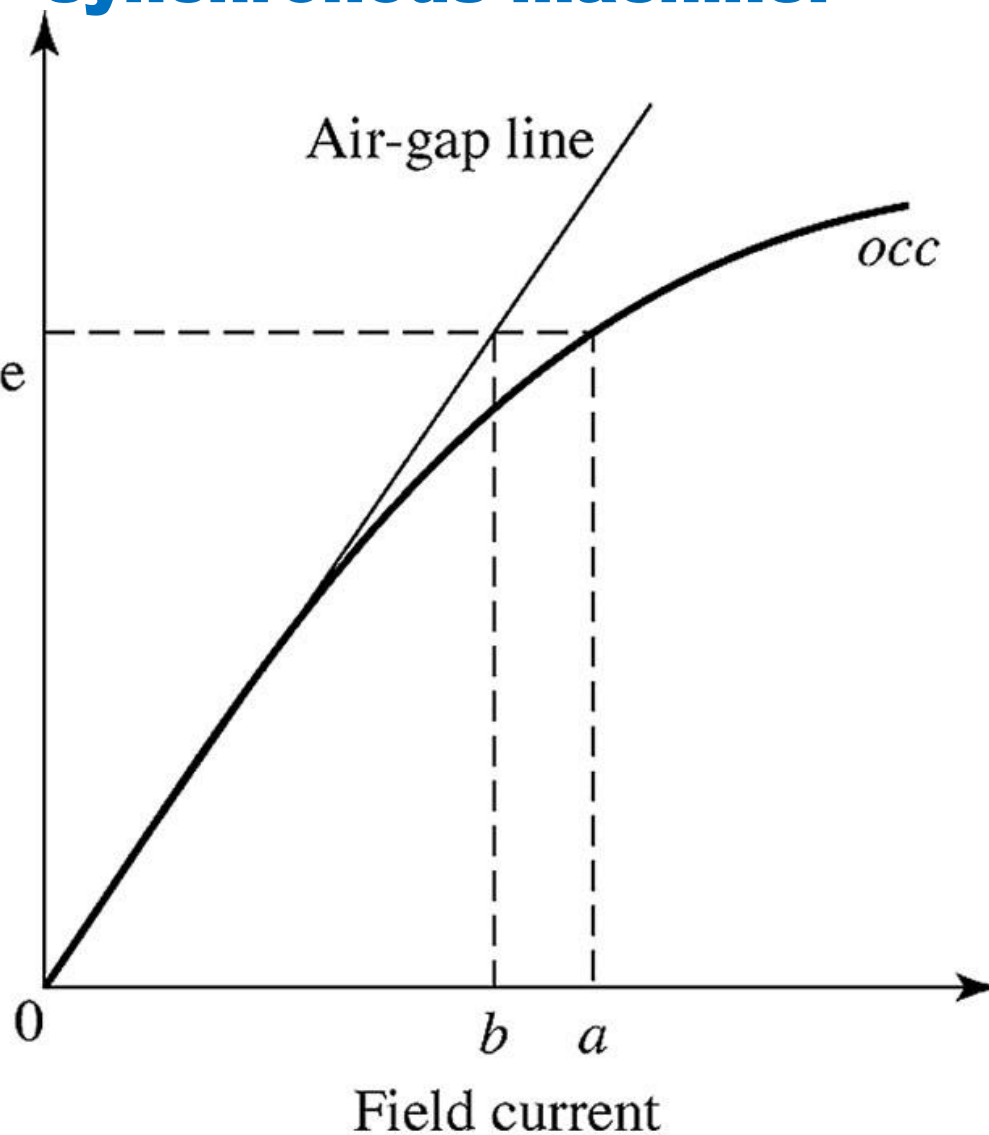


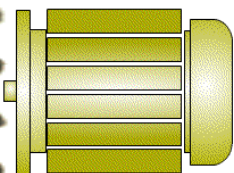
**Open-Circuit Characteristic (O.C.C.)**



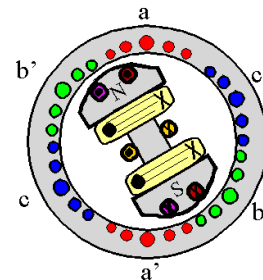
# Open-circuit characteristic of a synchronous machine.

Open-circuit  
armature voltage

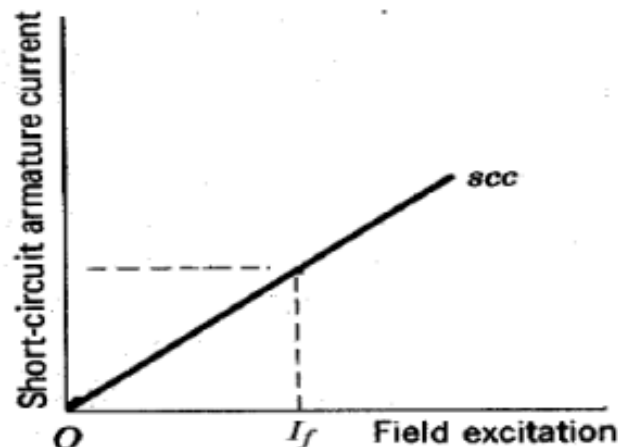
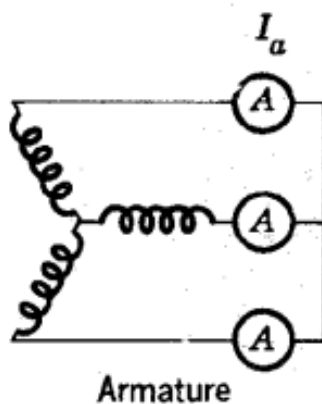
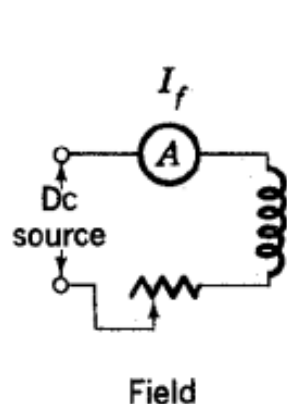




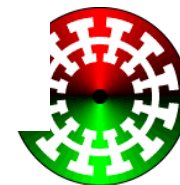
# SHORT CIRCUIT TEST (SCC)



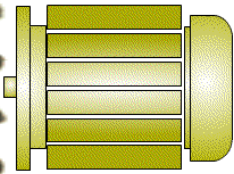
We conduct next the **short-circuit test** on the synchronous generator: the generator is rotated at the rated speed, all the terminals are short-circuited through ammeters, the field current  $I_F$  is set to **zero** first. Next, the field current is **increased in steps** and the armature current  $I_A$  is measured as the field current is increased. The plot of armature current (or line current) vs. the field current is the **short-circuit characteristic (SCC)** of the generator.



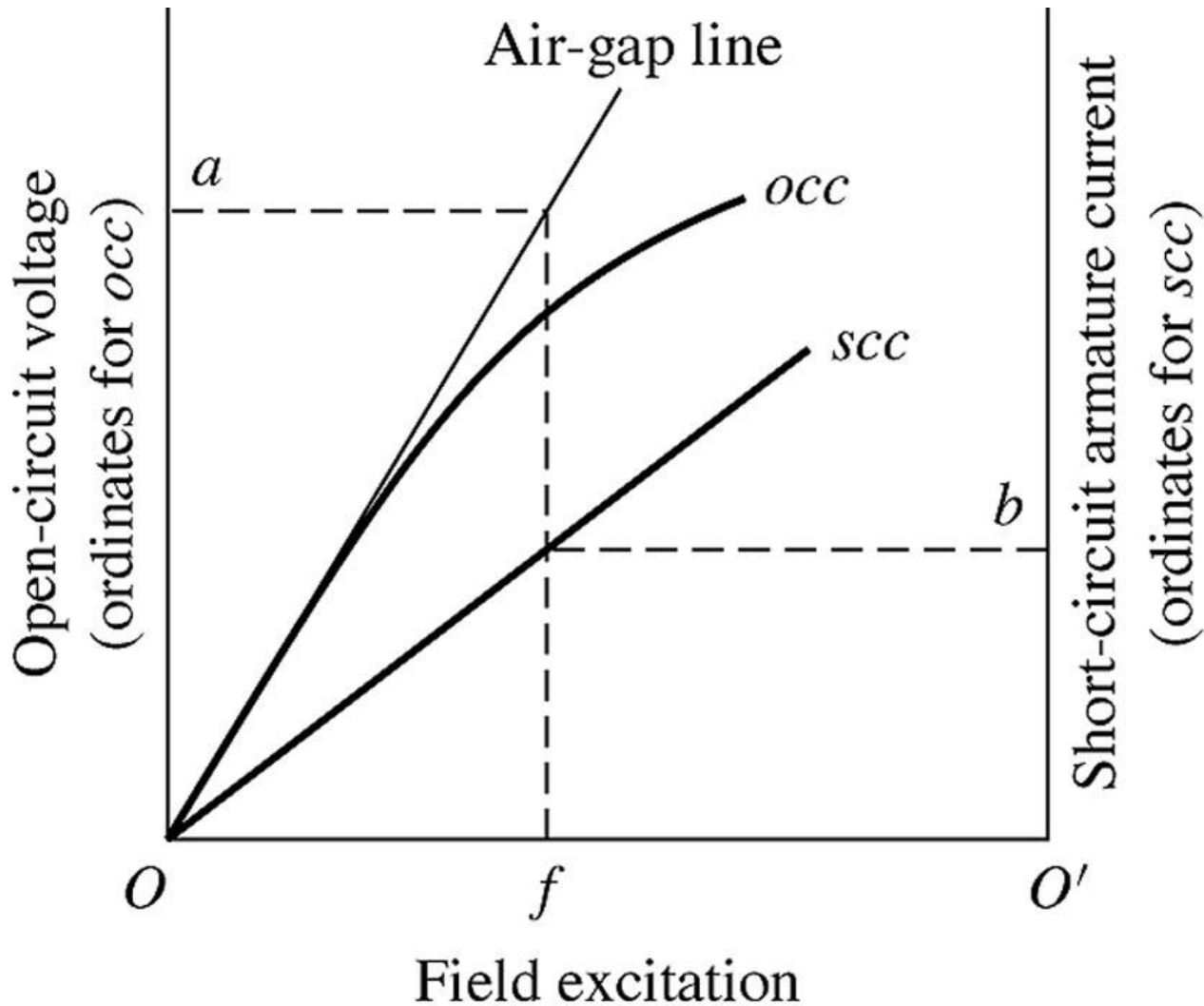
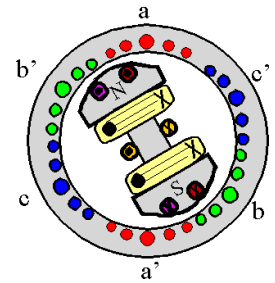
Short-circuit characteristics S.C.C.

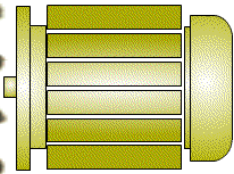




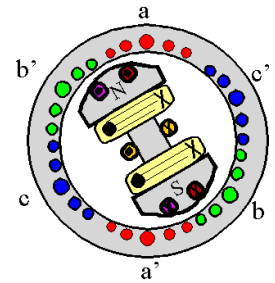


# Open- and short-circuit characteristics of a synchronous machine.



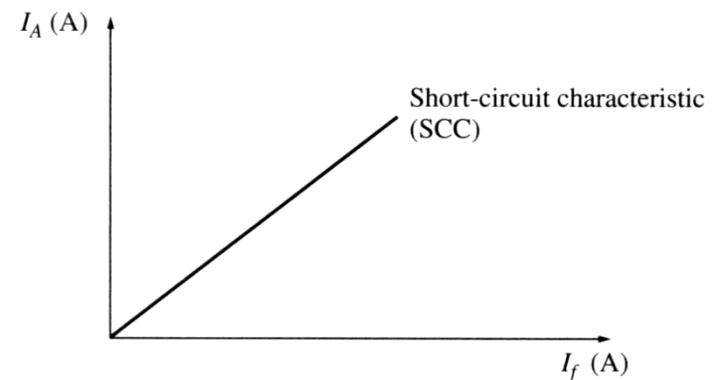


# Measuring parameters of synchronous generator model

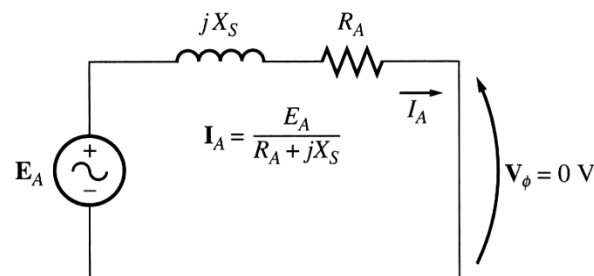


The SCC is a straight line since, for the short-circuited terminals, the magnitude of the armature current is

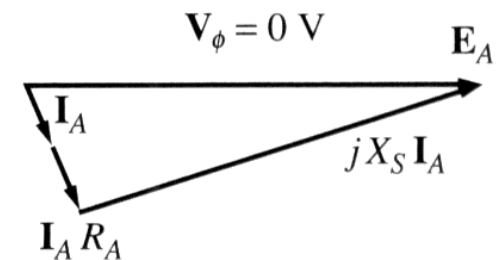
$$I_A = \frac{E_A}{\sqrt{R_A^2 + X_S^2}} \quad (20)$$



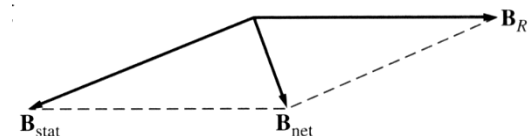
The equivalent generator's circuit during SC



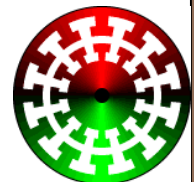
The resulting phasor diagram

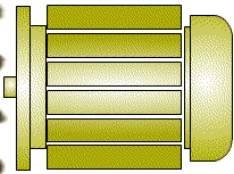


The magnetic fields during short-circuit test

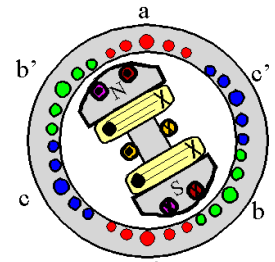


Since  $B_S$  almost cancels  $B_R$ , the net field  $B_{net}$  is very small.





## Measuring parameters of synchronous generator model



An approximate method to determine the synchronous reactance  $X_S$  at a given field current:

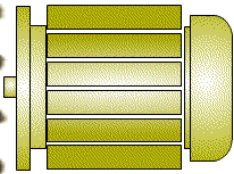
1. Get the internal generated voltage  $E_A$  from the OCC at that field current.
2. Get the short-circuit current  $I_{A,SC}$  at that field current from the SCC.
3. Find  $X_S$  from

$$X_S \approx \frac{E_A}{I_{A,SC}}$$

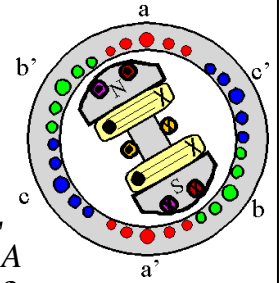
Since the internal machine impedance is

$$Z_S = \sqrt{R_A^2 + X_S^2} = \frac{E_A}{I_{A,SC}} \approx X_S \quad \left\{ \text{since } X_S \gg R_A \right\}$$





# Measuring parameters of synchronous generator model



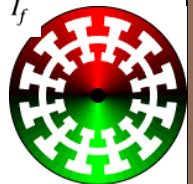
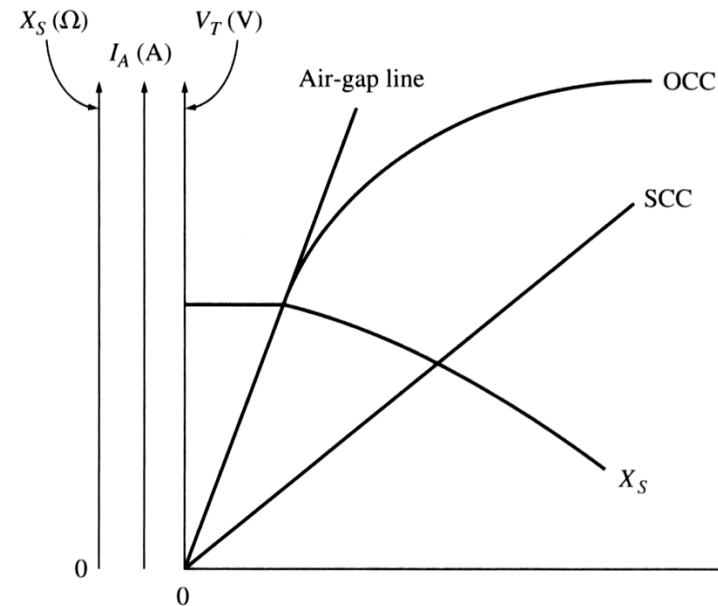
A drawback of this method is that the internal generated voltage  $E_A$  is measured during the OCC, where the machine can be saturated for large field currents, while the armature current is measured in SCC, where the core is unsaturated. Therefore, this approach is accurate for **unsaturated cores** only.

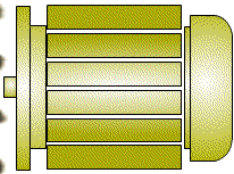
The approximate value of synchronous reactance varies with the degree of saturation of the OCC.

Therefore, the value of the synchronous reactance for a given problem should be estimated at the approximate load of the machine.

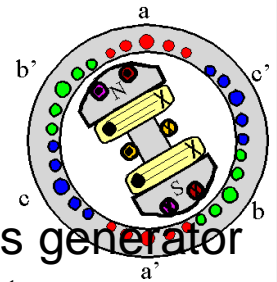
The winding's resistance can be approximated by applying a DC voltage to a stationary machine's winding and measuring the current.

However, AC resistance is slightly larger than DC resistance (skin effect).





# Measuring parameters of synchronous generator model: Ex



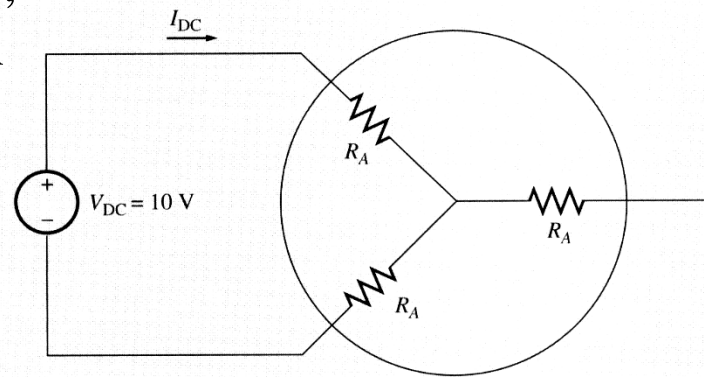
**Example** : A 200 kVA, 480 V, 50 Hz, Y-connected synchronous generator with a rated field current of 5 A was tested and the following data were obtained:

1.  $V_{T,OC} = 540$  V at the rated  $I_F$ .
2.  $I_{L,SC} = 300$  A at the rated  $I_F$ .
3. When a DC voltage of 10 V was applied to two of the terminals, a current of 25 A was measured.

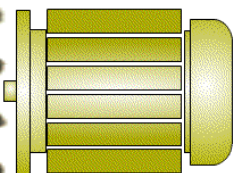
Find the generator's model at the rated conditions (i.e., the armature resistance and the approximate synchronous reactance).

Since the generator is Y-connected, a DC voltage was applied between its *two* phases. Therefore:

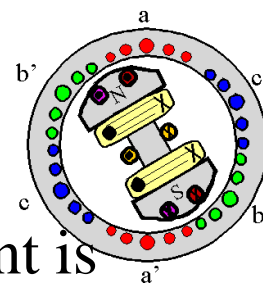
$$2R_A = \frac{V_{DC}}{I_{DC}}$$
$$R_A = \frac{V_{DC}}{2I_{DC}} = \frac{10}{2 \cdot 25} = 0.2 \Omega$$







## Measuring parameters of synchronous generator model: Ex



The internal generated voltage at the rated field current is

$$E_A = V_{\phi, OC} = \frac{V_T}{\sqrt{3}} = \frac{540}{\sqrt{3}} = 311.8 \text{ V}$$

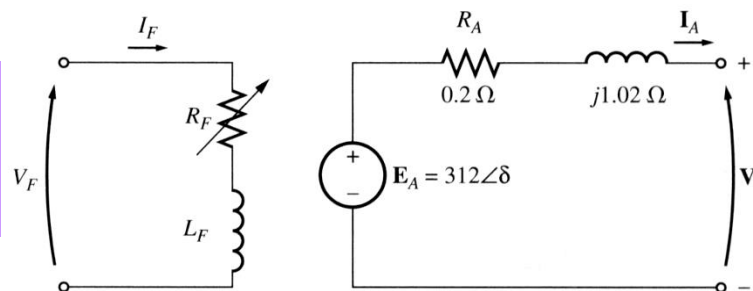
The synchronous reactance at the rated field current is precisely

$$X_S = \sqrt{Z_S^2 - R_A^2} = \sqrt{\frac{E_A^2}{I_{A, SC}^2} - R_A^2} = \sqrt{\frac{311.8^2}{300^2} - 0.2^2} = 1.02 \Omega$$

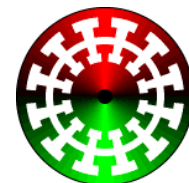
We observe that if  $X_S$  was estimated via the approximate formula, the result would be:

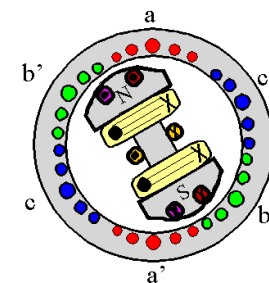
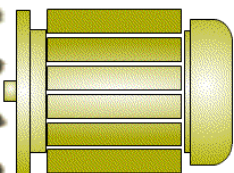
$$X_S \approx \frac{E_A}{I_{A, SC}} = \frac{311.8}{300} = 1.04 \Omega$$

Which is close to the previous result. The error ignoring  $R_A$  is much smaller than the error due to core saturation.

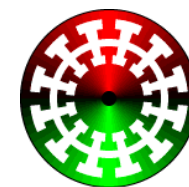


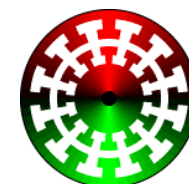
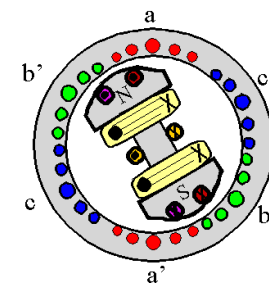
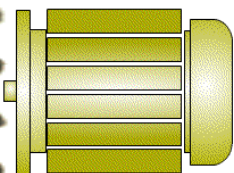
The equivalent circuit





PresenterMedia





A spiral-bound notebook with a light beige, textured cover. The metal spiral binding is visible along the left edge. The text "END OF LECTURE 13" is printed in a bold, blue, sans-serif font across the center of the cover.

**END OF LECTURE 13**