

## EE552 ELECTRICAL MACHINES III

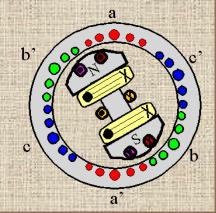
**LECTURE 3** 

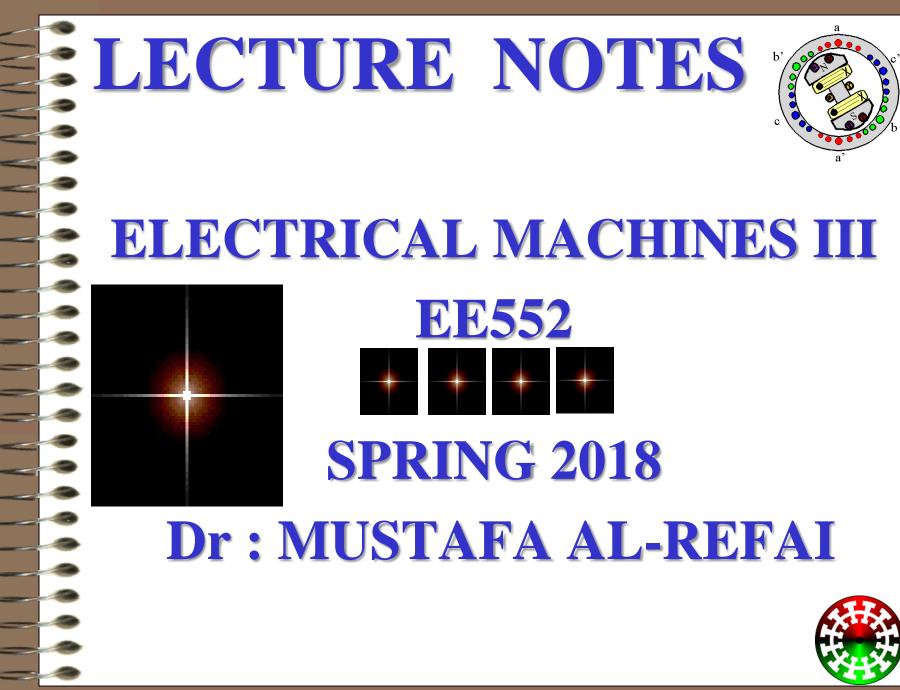




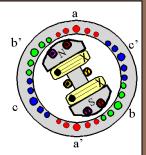


**10** 





**EE552 SPRING 2018** 



## **LECTURE 3**

### **AC MACHINERY FUNDEMENTALS**



**EE552 SPRING 2018** 

**DR**. MUSTAFA AL-REFAI

#### **AC MACHINERY FUNDEMENTALS**

# Producing Rotating Magnetic

**Reversing Direction of Magnetic Field Rotation** 

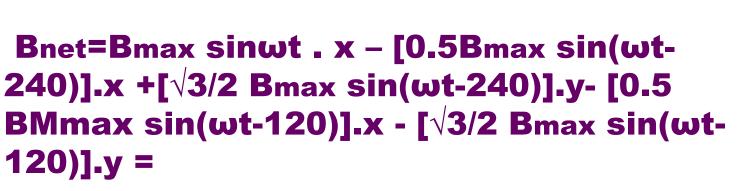
- if current in any 2 of 3 coils is swapped, direction of magnetic field's rotation will be reversed
- This means it is possible to reverse the direction of rotation of ac motor by switching connections on any 2 of 3 coils
  - This will be verified here
  - Bnet=Baa'(t)+Bbb'(t)+Bcc'(t)=Bmax sinωt /\_0° +

Bmax sin( $\omega$ t-240°) /\_120° +Bmax sin( $\omega$ t-120°) /\_240° Now each of the 3 components of magnetic fields

can be broken down into x & y components



#### AC MACHINERY FUNDEMENTALS Producing Rotating Magnetic Field



= (1.5 Bmax sinωt).x + (1.5 Bmax cosωt).y

Means: by swapping 2 of the 3 coils, B has same magnitude while rotating in a clockwise direction



# AC MACHINERY FUNDEMENTALS

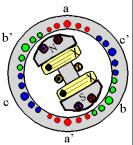
- In previous demonstration of 3 phase stator, B direction produced by coil wire assumed perpendicular to plane of coil (B direction by R.H.R. & in free space)
  - B in a real machine doesn't behave in simple manner assumed, since ferromagnetic rotor is in center of machine with a small air gap in between
  - Rotor can be cylindrical , with non-salient poles or with salient poles



## **SAC MACHINERY FUNDEMENTALS MMF & B Distribution on ac** machines □ An ac machine with: cvlindrical rotor & salient-pole (a) (b)

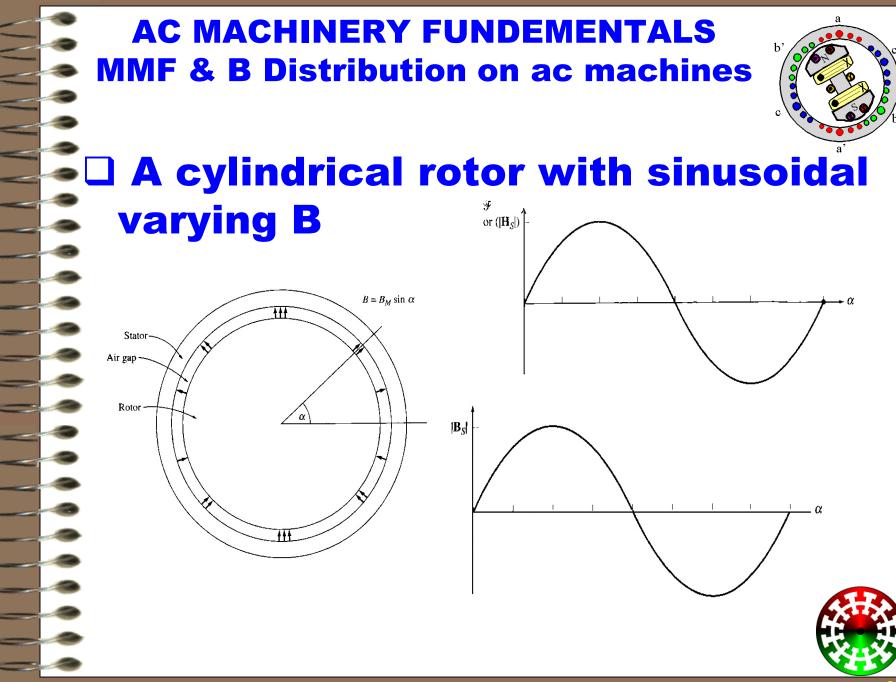
**EE552 SPRING 2018** 

#### **AC MACHINERY FUNDEMENTALS** MMF & B Distribution on ac machines

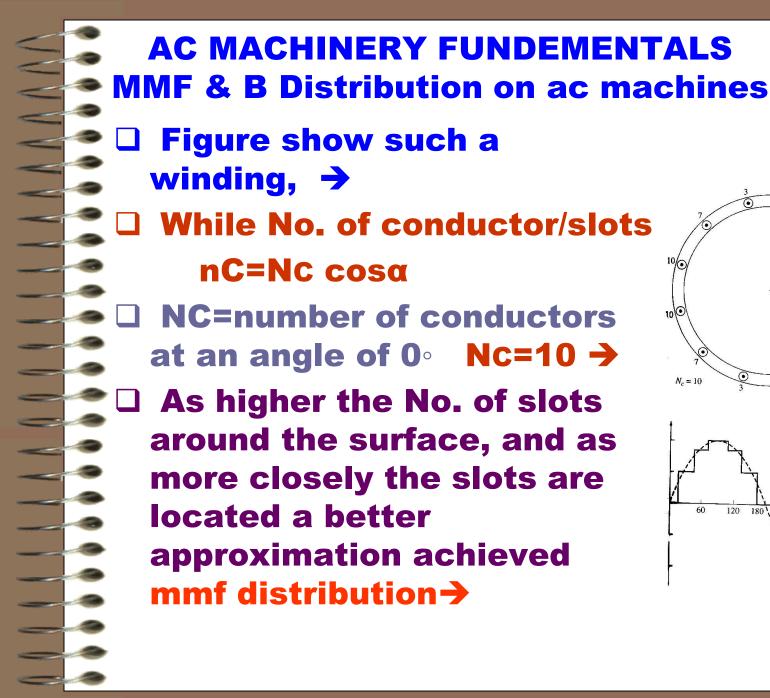


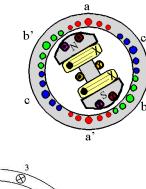
- **Discussion here is restricted to cylindrical rotors**
- Reluctance of air gap in this machine >> Reluctance of either rotor or stator,
  - → B takes shortest possible path across air gap & jumps perpendicularly between rotor & stator
- To develop a sinusoidal voltage in this machine, **B** should vary sinusoidally along the surface of air gap
- it needs **H** to vary sinusoidally,
- Easiest way is to distribute turns of winding among the slots around surface of machine in a sinusoidal manner

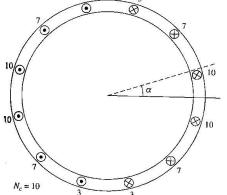


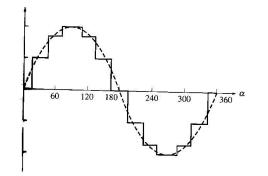


**EE552 SPRING 2018** 



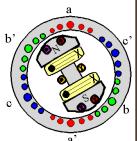








#### **AC MACHINERY FUNDEMENTALS** MMF & B Distribution on ac machines



In practice can not distribute windings exactly in accordance to last equation, since No. of slots is limited & only integral No. of conductors are available in each slot

The Resultant mmf approximately sinusoidal
Some higher order harmonic components present

Fractional-pitch windings employed to suppress unwanted harmonic components.

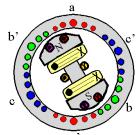
full pitch: if stator coils stretches across an angle same as pole pitch (360/p).

In **design** convenient to include **equal number of conductors** in each slot rather than varying **them**.

Then stronger higher order harmonics are present in comparison to original designs

There are special harmonic-suppression
techniques to be employed.





❑ As a 3 phase set of currents in a stator → rotating magnetic field

- A rotating magnetic field → a 3 phase set of voltages in coils of a stator.
- Equations governing induced voltage in 3 phase stator winding developed in this section.
- Starting with a single turn coil and expanding it to a general 3 phase stator.





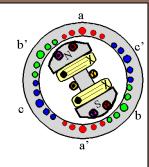
#### Induced voltage in a coil on a 2 pole stator

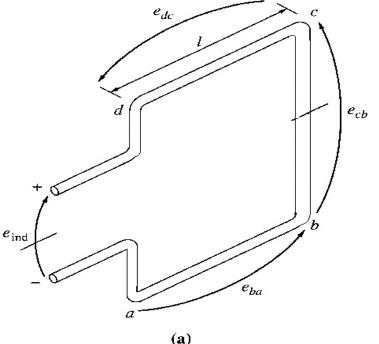
Figure in Next slide show a rotating rotor with a sinusoidally distributed B, Its stationary stator coil

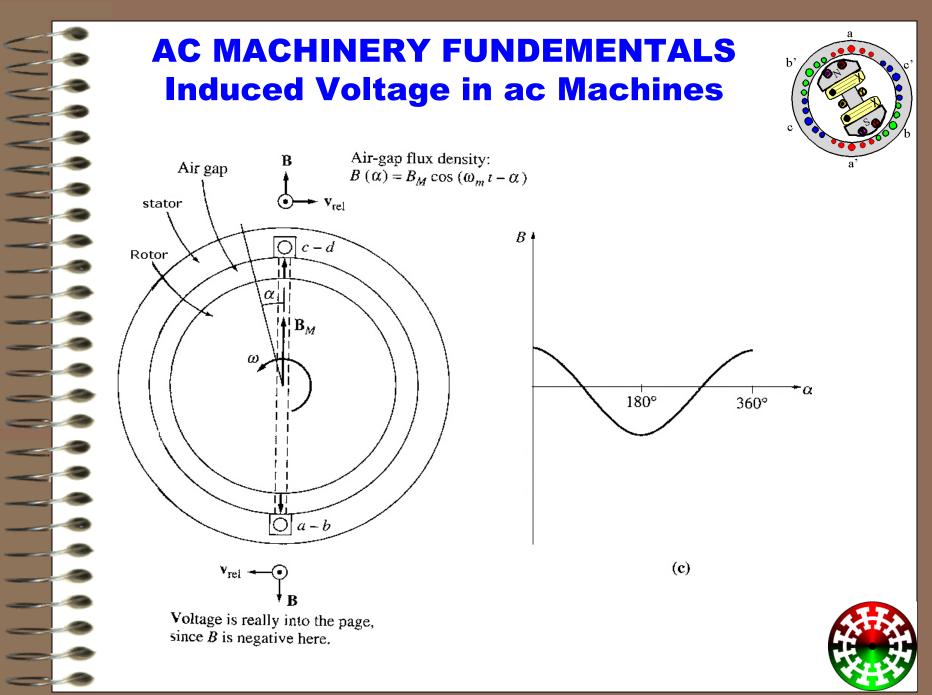
\* reverse of having a stationary magnetic field & rotating loop velocities shown w.r.t. a

frame of reference in which B is stationary

(i.e. a frame rotating with the same speed as rotating field)



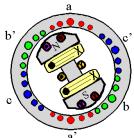




**EE552 SPRING 2018** 

#### DR. MUSTAFA AL-REFAI



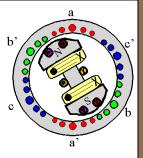


- Assuming magnitude of B produced by rotor in air gap varies sinusoidally with mechanical angle
- B always radially outward,
- α angle measured from direction of peak rotor B
  - $B = B_{max} \cos \alpha$
- Note: in some locations would be toward rotor when its value is negative
- since rotor is rotating at an angular velocity ω<sub>m</sub>, magnitude of B at any angle α around stator as function of time is:

B= Bmax cos (ωm t-α)

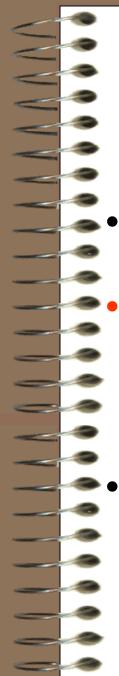


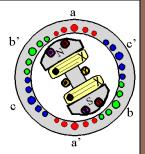




- The induced voltage is :
  - e=(v x B) . I
  - v= velocity
  - **B= magnetic flux density vector**
  - I= length of conductor in the magnetic field
  - **Derived for moving wire in stationary magnetic field**
  - Here the wire is stationary & magnetic field is moving, a vrel can be employed (using the magnetic field as reference frame)



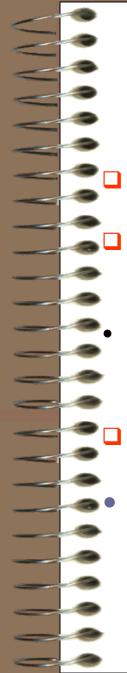


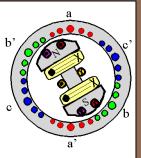


- Total voltage induced in coil, is sum of voltages induces in each of four sides:
  - **Segment ab:** For ab α=180° Assuming B directed radially outward from rotor, angle between V & B in segment ab is 90° while VxB is in direction of I, so:
  - **e**ba **=(v x B). I =vBI** directed out of page
    - = -V [Bmax cos(ωmt-180°)] I

= - V Bmax I cos(ωmt-180°)







segment bc: since V x B for this segment is perpendicular to I, voltage on this segment is zero  $ecb=(V \times B) \cdot I=0$ segment cd: for this segment  $\alpha=0^\circ$ , and B directed outward from rotor, angle between V and B in segment cd is 90°, while quantity VxB is in direction of I,

- edc = (VxB).I
  - **=vBI** directed out of the page
  - =v (Bmax cosωmt) l =v Bmax l cosωmt

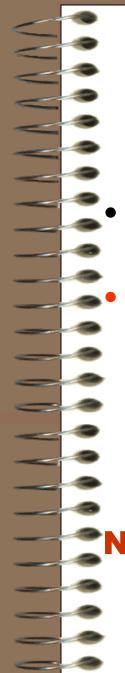
**segment da** : voltage on segment da is zero, since vector quantity VxB perpendicular to | ead=(VxB).I=0

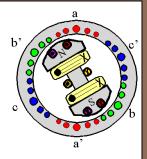
Eind = eba+edc=

-vBmaxicos(ωmt-180°)+vBmaxicosωmt=2 vBmax icosωmt=

= 2(rωm)Bm I cos ωmt= 2 r I Bm ωm cosωmt





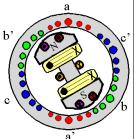


- flux passing through coil is  $\varphi$ =2rlB<sub>max</sub>, while  $\omega_m = \omega_e = \omega$  for a 2 pole stator
- induced voltage can be expressed as:
  - $e_{ind} = \varphi \omega cos \omega t$  in a single turn
  - if stator has Nc turns of wire
  - $e_{ind} = Nc \phi \omega cos \omega t$

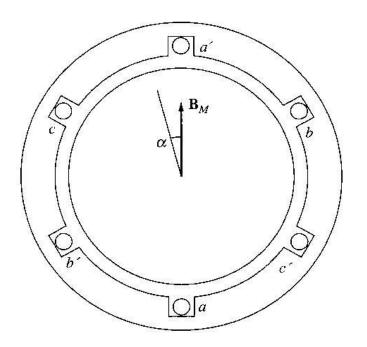
Next: induced voltage in a 3 phase set of coils computed







- 3 coils, each of NC turns, placed around rotor
- Voltage induced equal magnitude, 120° different in phase





EE552 SPRING 2018

DR. MUSTAFA AL-REFAI



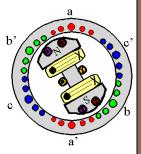
- eaa =NC φωsinωt V
- ebb =NC φωsin(ωt-120°) V
- ecc =NC φωsin(ωt-240°) V
- **Therefore:** 
  - a 3 ph. currents generate uniform rotating magnetic field in stator air gap

and a uniform rotating magnetic field can generate a 3 ph. Set of voltages in stator

The RMS Voltage in 3 ph. Stator

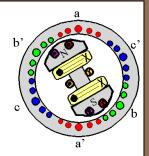
Peak voltage in any phase of this 3 ph. Stator is: Emax=NC  $\varphi \omega$  & since  $\omega = 2\pi f \rightarrow$ Emax=2  $\pi$  NC  $\varphi f$ 





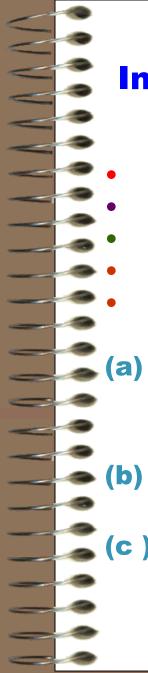
- rms voltage of each phase is:  $E_A = \sqrt{2\pi Nc} \phi f$ 
  - rms voltage at terminals of machine depend on whether stator is Y or Δ connected
  - Terminal voltage for Y connected  $\sqrt{3}$  EA and for A connected is EA

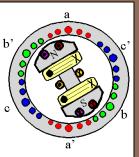




- For a simple 2 pole generator, Bmaxrotor=0.2T, ωm=3600 r/min
- Stator diameter 0.5 m, its coil length 0.3 m, and there are 15 turns per coil
- Machine is Y connected
- what are 3 ph. Voltages of gen. as **(a)** function of time
- what is rms ph. Voltage of gen. ? **(b)**
- what is rms terminal voltage of **(C)** generator?





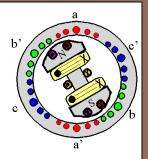


#### **Solution:**

- φ=2.r.l.B=d.l.B
- d= diameter , I=length of coil loop
- Flux in machine: φ=(0.5)(0.3)(0.2)=0.03 Wb
- **Speed of rotor is: ω=(3600)(2π)(1 min/60)=377** rad/s
- Emax=NCφω=(15)(0.03)(377)=169.7 V
- 3 ph. Voltage: eaa'=169.7 sin 377t V, ebb'=169.7 sin (377t-120°) V, ecc'=169.7 sin (377t-240°) V
- ) rms phase Voltage of generator: EA=Emax/ $\sqrt{2}$  = 169.7/ $\sqrt{2}$  =120 V
- (c) Since generator is Y connected :  $VT=\sqrt{3}EA=\sqrt{3}(120)=208 V$



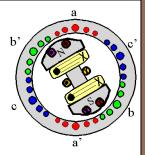




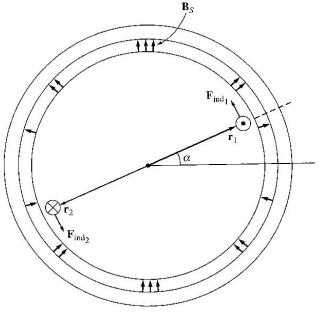
- 2 magnetic fields present in a ac machine under normal operating conditions:
- (a) a magnetic field from rotor circuit
- (b) another magnetic field from stator circuit
- Interaction of 2 magnetic fields produces torque in machine
  - similar as 2 permanent magnets near each other will experience a torque causes them to line up







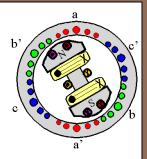
- Fig. shows a simplified ac machine, with:
- a sinusoidal stator flux distribution peaks in upward direction &
- a single coil or wire mounted on rotor
- stator flux distribution Bs(α)=Bs sinα
- assuming: when Bs positive, B points radially outward from rotor surface to stator surface



 $|\mathbf{B}_{S}(\alpha)| = B_{S} \sin \alpha$ 







- applied force on each conductor of rotor: force on conductor 1 located perpendicular to page:
  - F=i(lxB)=ilBs sinα direction shown in last figure

torque :Tapplied=(rxF)=r.i.l.Bs sinα counterclockwise

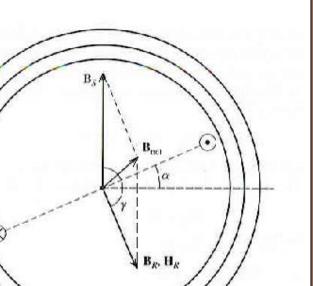
therefore: Torque on rotor loop is:

Tapplied=(rxF)=2rilBs sinα counterclockwise



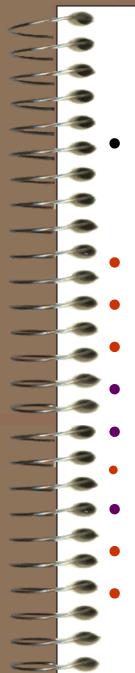


- Alternatively this equation can be determined through below figure also:
- 1- i flowing in rotor coil produces HR = C i
  - **C** : a constant
- 2- angle between peak of Bs & peak of HR is γ and
- γ=180-α, sinγ=sin(180α)=sinα
- Combining these 2 observations: Torque on loop is:
  - Tapp=K HR Bs sinα counterclockwise

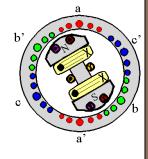




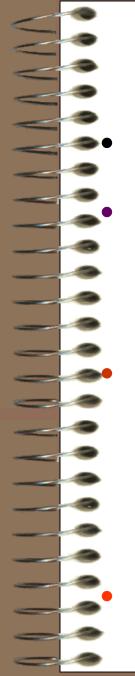
 $y = 180^{\circ} - \alpha$ 



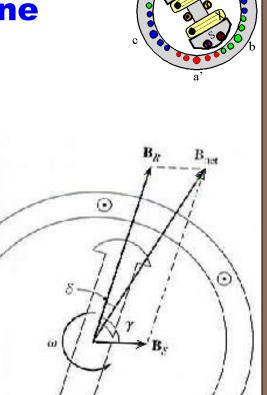
- where:
  - K, constant dependent on machine construction
- Tapp=K (HR x Bs)
- since Br=µ Hr it can be reordered as :
- Tapp=k (Br x Bs) (where: k=K/µ)
- The net flux density in machine:
- Bnet=BR+BS → BS = Bnet BR
- T=k BR x (Bnet BR)=k(BR x Bnet) k(BR x BRapp)
- The 2<sup>nd</sup> term is always zero →
- Tapp=k Br x Bnet or Tapp=k Br Bnet Sinδ
- δ: angle between BR and Bnet







- Figure: is an example of one application
  - Its magnetic fields rotating in counterclockwise direction, shown through direction of rotation
    - While the direction of applied torque on machine by applying Right Hand Rule to the last equation is clockwise or opposite to direction of rotation
  - **Conclusion:** Machine must be acting as a **Generator**

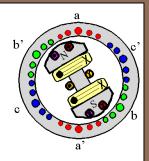


3











EE552 SPRING 2018





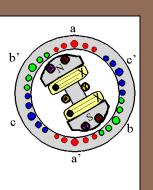


Presenterfledia

PresenterMedia







EE552 SPRING 2018

#### DR . MUSTAFA AL-REFAI

32

